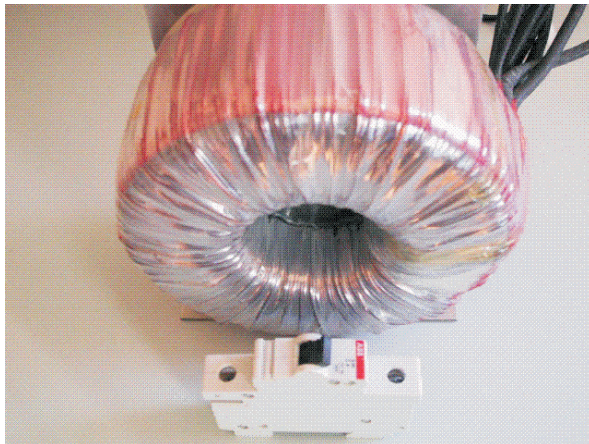


## current inrush avoider for toroidal-transformers



Picture 1 shows a 1 kVA, 230 V toroidal core transformer and a C 4 A power circuit-breaker. The toroidal core transformer has low losses and a nominal current of 4,3 Aeff, but an inrush current of 56 times of the nominal current = 240 Aeff. The C 4 A line protector switch trips when 6 times of the nominal current flows = 24 Aeff. The inrush current of the transformers is 10 times higher. Conclusion: The toroidal core transformer and the power circuit-breaker are not combinable.

It's a pity, that both mismatch. Each of them has advantages of it's own. The low loss transformer is energy-saving, remains cold and has a very low no-load current of only 25 mA.

The C 4A line protector switch is able to protect the transformer together with long wires behind him.

(When a short circuit occurs at the end of the long wires behind the transformer, then the short circuit currents are low and must trip the line protector switch).

In a factory area or inside of large buildings such long wires are commonly. They are supplying any actuator with 24V AC for example. Up to now big wire sizes were used for low resistance to enable the short current flowing is high enough to trip the fuse in a short time before the cable is burning.

Additionally a secondary side fusing must be spent.

But thick cables are expensive. For this reason, when a so called soft short circuit occurs, the inner resistance of the transformer should be as low as possible.

This allows again thinner wires behind the transformer.

- But this raises the inrush current, when the inner resistances of the transformer are low.

Because the sum of all resistances in the circuit between fuse and short circuit limits the short circuit current, which must trip the fuse in a short time less than 200 milliseconds.

But with a low inrush transformer it is paradox.

The copper inside of the transformer must be spent many times for the cables behind the transformer, when they are longer than 100 m and more. And the customer pays the bill.

However, when a so called „transformer-switching-relay“ is placed between the both in the picture 1, then the transformer and the line protect switch are consistent.

The transformer switching relays avoid the inrush current in all circumstances better than normally used inrush current limiters.

Sometimes so called inrush current limiters, cannot limit the inrush current in all circumstances.

They can't stand being turned on short after short circuits.

Mostly they consist of a bridged NTC or fix resistor.

After a short power line interruption they cannot limit the inrush currents, when the power line voltage comes back.

Normally used EI core control-transformers run hot even in no load state.

The reason is in the construction.

- Either a transformer has low losses or he has a low inrush current. Both together is not possible with normal costs.

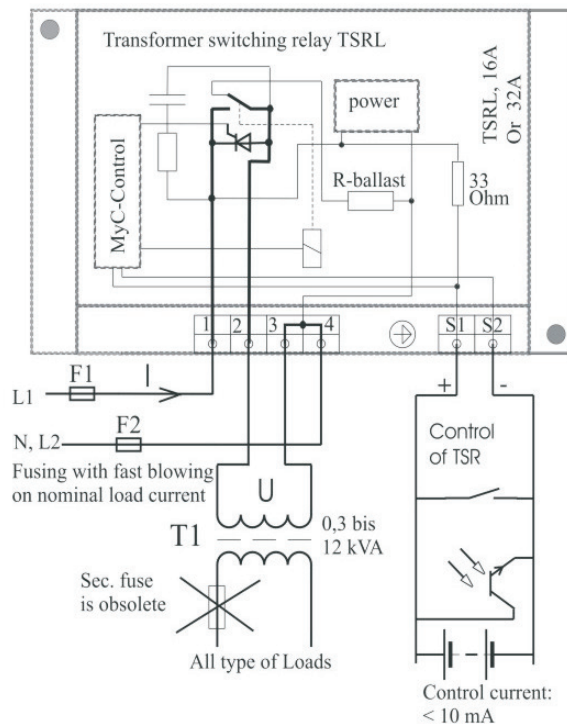
With the argument for transformers with low inrush currents on correspond the argument of an easy to fuse of the transformer. That's often published. But nobody mentions the higher warming up and the higher current losses of these kinds of low inrush transformers.

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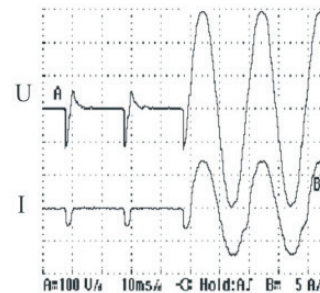
# current inrush avoider for toroidal-transformers

## Transformer switch on without inrush current peaks

Inrush current avoiding with a TSR  
Transformer switching relay  
Switch full on after premagnetising  
of the transformer



Switched on with load with a TSRL



$I_{peak} = I_{nom} = 7A_{peak}$   
= current of nominal load

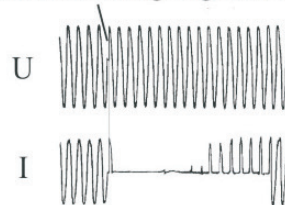
Switch on in no load state

U

I

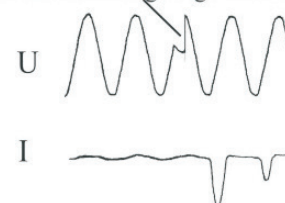
$I_{max.} = I_{no\ load}$   
(visible is a typically no load current)

Reaction on voltage sags with TSR



$I_{max.} = I_{nominal}$   
also available with fast switch on.

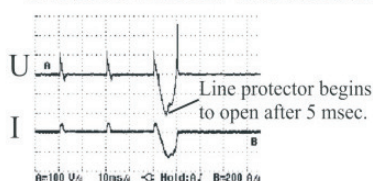
Reaction on voltage sags without TSR



$I_{max.} = U_{peak} \div \text{with}$   
(R line + R copper prim.)  
= 200 A peak,  
each fuse is blowing then

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Switch on with short circuit after transfo



A 16A B-typ line protector  
trips directly after switch on.  
No damage of TSRL until 400A  
for 10msec.

### Advantages with a TSR:

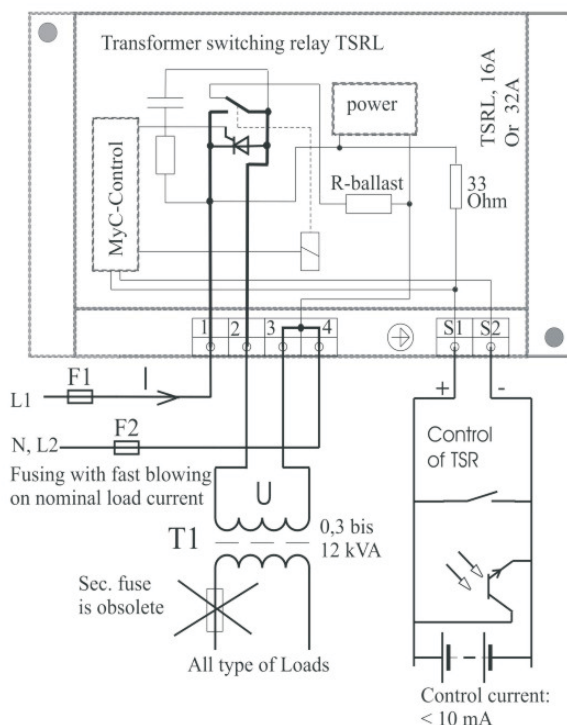
- No limit in repetition of switching, no waiting time.
- Fast blowing fuses with nominal current value useful.
- No overheating of transformer
- No damage when short circuit by correct fusing
- Avoid inrushes after voltage sags and dips.
- Allows transformers with low losses and max. Induction.
- Replace contactor and inrush current limiter and saves money in cases when transformer must be switched often.

Picture 4.

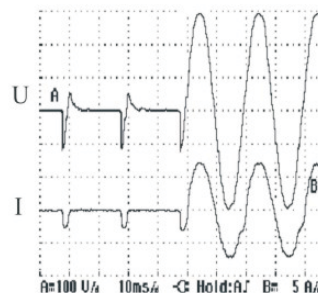
# current inrush avoider for toroidal-transformers

## Transformer switch on without inrush current peaks

Inrush current avoiding with a TSR  
Transformer switching relay  
Switch full on after premagnetising  
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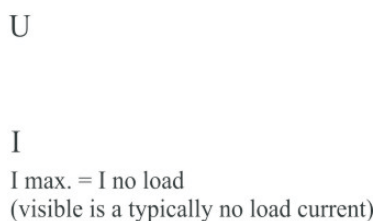


Switched on with load with a TSRL

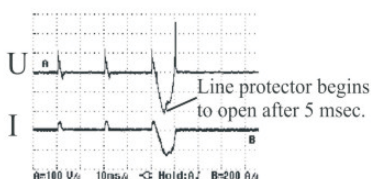


$I_{peak} = I_{nom} = 7A_{peak}$   
= current of nominal load

Switch on in no load state



Switch on with short circuit after transfo

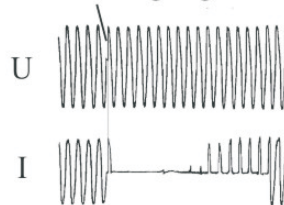


A 16A B-type line protector trips directly after switch on.  
No damage of TSRL until 400A for 10msec.

### Advantages with a TSR:

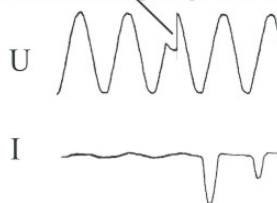
- No limit in repetition of switching, no waiting time.
- Fast blowing fuses with nominal current value useful.
- No overheating of transformer
- No damage when short circuit by correct fusing
- Avoid inrushes after voltage sags and dips.
- Allows transformers with low losses and max. Induction.
- Replace contactor and inrush current limiter and saves money in cases when transformer must be switched often.

Reaction on voltage sags with TSR



$I_{max.} = I_{nominal}$   
also available with fast switch on.

Reaction on voltage sags without TSR



$I_{max.} = U_{peak} \text{ div. with } (R_{line} + R_{copper \text{ prim.}})$   
= 200 A peak,  
each fuse is blowing then

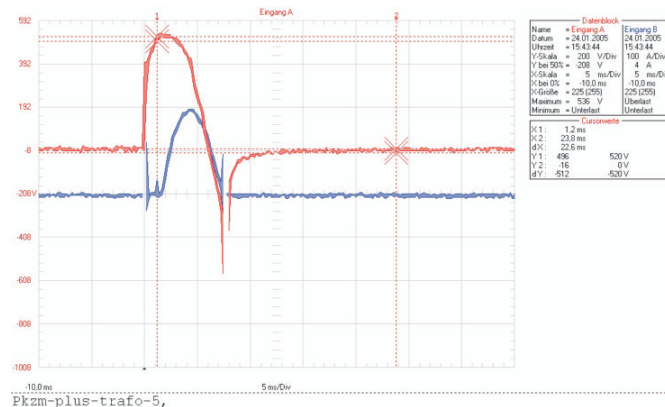
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Picture 4.

## current inrush avoider for toroidal-transformers

How it runs switching on without a TSRL?

The graph in the bottom shows the switch on Voltage and current, when a 1kVA toroidal core transformer is switched on by a electro-mechanical contactor. He is fused with a PKZM0-4-T line breaker especially for transformers.



Picture 5.

(Switch on directly.)

Input A, top= Voltage at the transformer, Input B, bottom = current into the transformer.

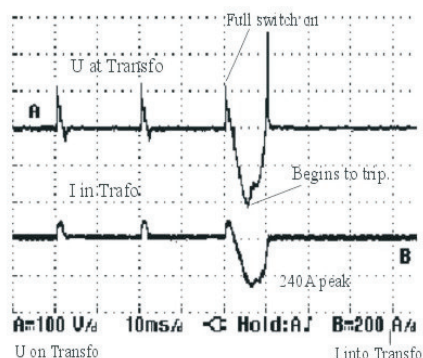
The line protector trips within 10 Milliseconds.

The low loss Transformer has an air gap-less Iron core. He produce a inrush current of 200A peak, thats 140Aeff. ( Thats the 56 times of nominal current.)

Line protector switches who have a short circuit breaker current of more than 22 times of the nominal current are not available. They'd not be able to protect the wires when a so called soft short circuit occurs.

TSRL switch on to a short circuit at his output

Fused with a 16A B-Type circuit breaker:  
He trips after full switch on.  
(A R-Type-10A circuit breaker would trip while  
premagnetising.) TSRL withstands this short circuit.



Picture 6.

When between circuit breaker and 1kVA transformer a TSRL is placed:

Channel A shows the voltage on the transformer, channel B shows the Amps into the transformer. The circuit breaker start to trip in the peak of the current after 5 msec. Only 240Amps peak are flowing. The TSRL withstands 1000Amps peak for 10 msec.

Switch on onto short circuits is no problem for the TSRL.

## current inrush avoider for toroidal-transformers

When the TSR switches on to a short circuit after the transformer he gets no damage, when the fusing is correct.

Other inrush current limiters failed this test.

Additionally: A TSRL with the option for fast recognition of so called fast voltage dips can avoid inrushes and fuse tripping when tested the equipment with EN 61000-4-11. This TSRL has also a switch off threshold from 170Veff and a switch on threshold from 185Veff.

When voltage sags occurs, no jitter with mechanical contactors is induced when a TSRL is in front of a control transformer.

A separately voltage Supervisor relay is no more needed than.